NFARL September 2009 HF Antennas FOR HF Beginners

## What we will cover.

# A little theory Types of antennas suited for beginners Some antenna show and tell

**IF YOU DON'T REMEMBER ANYTHING ELSE** FROM TONIGHT. REMEMBER THESE **THREE THINGS!** 

1.

## ALL MULTIBAND ANTENNAS ARE A COMPERMISE IN SOME PARAMETER!



## There ain't no free lunch.

3.

## You get nothing for nothing!

## Santa Claus is DEAD!



Band	1/8 WL	1/4 WL	1/2 WL	1WL	2 WL	3 WL	10 WL
160	68 Ft.	136 Ft,	273 Ft.	546 Ft	1092 F	t1638 F	<b>t5460 F</b> 1
80	35 Ft	70 Ft	140 Ft	281 Ft	562 Ft	843 Ft	2810 F
40	17 Ft	35 Ft	70 Ft	140 Ft	280 Ft	420 Ft	1400 F
20	8 Ft	17 Ft	35 Ft	70 Ft.	140 Ft	210 Ft	700 Ft
17	6 Ft	13 Ft	27 Ft	54 Ft.	108 Ft	162 Ft	540 Ft
15	6 Ft	12 Ft	24 Ft	49 Ft.	98 Ft	147 Ft	490 Ft
12	5 Ft	10 Ft	20 Ft	39 Ft.	78 FT	117 Ft	390 Ft
10	4 F t	8 F t	17 Ft	35 Ft.	70 Ft	105 Ft	350 Ft



This is the conventional method of depicting signal reflection from the earth by assuming there is an image antenna below the surface and the same distance below the surgace as the real antenna is above the surface. By using a little geometry it can be shown that the reflected wave travels a greater distance, the distance is equal to the length of line BC, and this length determines the phase of the two signals at the distance point P. Each antenna, whether vertical or horizontal, has an effective height and this determines where the signal reflects from the earth. This usually occurs approximately 1.5 to 2 wave length from the antenna. The point I want to make is that nothing you do directly under the antenna, such as increased radial fields, will effect the signal reflection point. It may increase the efficiency of the antenna but, it will not help the reflected signal. The only way to do that is to make the first reflection occur over salt water.



Fig 1—Variation in radiation resistance of vertical and horizontal half-wave antennas at various heights above flat ground. Solid lines are for perfectly conducting ground; the broken line is the radiation resistance of horizontal half-wave antennas at low height over real ground.



Fig. 8 Current and voltage distribution along a half-wave dipole.



Fig. 9 Cross section of surface pattern for a half-wave dipole in space (based on horizonta) and vertical field patterns of dipole).



#### FEED LINE MATCHED LOSS

per 100 FT.

	1 MHZ	10MHZ	100MHZ
RG-213	0.2 db	0.6 db	1.9 db
LMR-500	0.1 db	0.4 db	1.2 db
RG-58A	0.4 db	1.3 db	4.5 db
CQ-553 Ladder Line	0.02 db	0.08 db	0.3 db

100 Wts input at 10 MHz Results in

#### Watts Out

RG-213	87.1
LMR-500	91.2
RG-58A	74.13
CQ-553	98.17



Fig 14—Additional line loss due to standing waves (SWR, measured at the load). See Fig 23 for matchedline loss. To determine the total loss in dB, add the matched-line loss to the value from this graph.











This is one method of handling bringing ladder line down the side of a tower. The stand offs are made of 1-1/2 inch PVC pipe cut 24-inches long and then a hole saw of 1-1/4 inch diameter is used to cut a hole through the middle of the PVC pipe. This gives you 2 pieces appoximately12-inches long with a half-moon on one end. This end will just fit around the leg of Rhon 25 tower. About 1/2-inch ahead of the half-moon cut a vertical slots on each side of the pipe that will allow a hose clamp to slide through. When this is placed around the leg of the tower and tightened it make a very stout stand-off.

On the other end cut a vertical slot deep enough to allow the ladder line to slide all the way in. Drill a 1/4-inch hole through the pipe at right angles to the slot. This will allow the use of a tie wrap to be used to hold the ladder line in the slot.

Give the ladder line about 1 twist per foot and this will keep the line from being whipped in the wind. It also allows the ladder line to have equal exposure on each wire to the tower .









EZNEC Pro/2





EZNEC Pro/2





1/2 WL Vertical Antenna

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### **Vertical Antenna**

#### "T" Antenna

Inverted "L"



**Loop Antennas** 

#### **DIPOLE ANTENNA WITH DIFFERENT FEEDS**



#### Feed 33% from end 60 foot

EZNEC Pro/2

3.8 MHz

72.0 deg.

6.23 dBi

0.0 dBmax



#### **Dipole Antenna with 3 Different Feeds on 20-Meters**



#### 3.8 MHz dipole on 14.2 MHz 33% feed

#### **3.8 MHz dipole on 14.2 MHz End feed**



#### Random Length wire 92-Feet long @ Appox. 45-Degrees



28.4 MHz Impedance = 712.2 + J 734.1 ohms



18.1 MHz Impedance = 252.5 + J 492.5 ohms Random Length wire 92 feet long @ Appox. 45-degree

* Total Field Horizontal Pol Vertical Pol			EZNEC Pro/2	Total Field	0 dB 	D	EZNEC Pro/2
Elevation Dist		Curoor Flou	35.0 dog			o ==	3.0 WITZ
Azimuth Angle	0.0 deg.	Cursor Elev Gain	25.0 deg. 0.58 dBi	Elevation Plot Azimuth Angle	0.0 deg.	Cursor Elev Gain	153.0 deg. 0.88 dBi
Outer Ring	0.58 dBi		0.0 dBmax	Outer Ring	0.88 dBi		0.0 dBmax
Slice Max Gain	0.58 dBi @ Elev Angle = 25.0 deg.			Slice Max Gain	0.88 dBi @ Elev Angle = 153.0 deg.		
Beamwidth Sidelebe Coip	45.4 deg.; -3dB @ 8.4, 53.8 deg. 0.58 dBi @ Elou Apolo = 154.0 dog			Beamwidth	51.1 deg.; -3dB @ 120.2, 171.3 deg.		
Eront/Sidelobe	0.36 dbi @ Elev Angle = 134.0 deg. 0.0 dB			Sidelobe Gain Exect/Sidelobe	-0.16 dBi @ Elev Angle = 26.0 deg.		
110111010101000	0.0 40			Fruitivaluelupe	1.04 GD		

80-Meter "T" Impedance = 27.46 - J 5.174 ohms

80-Meter Inverted "L" Impedance = 69.71 + J 315.9 ohms Now here to explain the Loop SkyWire and Loops in general is the originator of the Loop SkyWire Antenna

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Za is "reasonable" at ALL multiples (harmonics) of F



r= # ~ 78% of CIRCLE AREA

$$\lambda_{LOOP} = \frac{1005}{F_{mH_3}} \dots \text{Feet}$$



1 AA-X,  $X = X_1 + X_c$  $X_{c} \leq O$ X, ≥0 RESONANCE X = C



	note	==>>	==>>	Power T	ransfer v	vorksheet	<<==	
	Freq (mhz)	===>>		a alam anan kasa kasa kasa kasa alam				
A= B= C= D=	Total Line Attn Line (Zo) Load (R) Load (X)	(dB)   ohms   ohms   ohms	3.0 50.0 100.0 200.0	0.3 50.0 100.0 200.0	3.0 300.0 100.0 200.0	0.3 50.0 100.0 200.0	3.0 450.0 100.0 200.0	
E= F= G= H= I=	Line Loss Fa Refl Coeff @ Load Load SWR (@ Refl Coeff @ I Input SWR (@sh	(ant) (ant) ant) nput ack)	0.501 0.825 10.40 0.413 2.41	0.944 0.825 10.40 0.778 8.03	0.5010.6324.440.3171.93	0.933 0.825 10.40 0.770 7.68	0.501 0.689 5.43 0.345 2.05	
] = = = = = = = = = = = = = = = = = = =	Fwd Power @ Input Power @ Load ( Power Reflected @ Pwr Return @ Input Net Power Out @ I Power Xfr to Load Transfer Ratio Total Power Loss Total Pwr Loss (S- Total Mismatch Los	(FWD) ant) Load (REF) nput (ant) (%) (dB) unit) s(dB)	$   \begin{array}{r}     100.0 \\     50.1 \\     34.1 \\     17.1 \\     82.9 \\     16.0 \\     19.3 \\     7.1 \\     1.2 \\     4.1 \\   \end{array} $	$   \begin{array}{r}     100.0\\     94.4\\     64.2\\     60.6\\     39.4\\     30.2\\     76.7\\     1.2\\     0.2\\     0.9   \end{array} $	No Cor 100.0 50.1 20.0 10.0 90.0 30.1 33.4 4.8 0.8 1.8	jugate Ma 100.0 93.3 63.5 40.8 29.9 73.2 1.4 0.2 1.1	100.0 50.1 23.8 11.9 88.1 26.3 29.9 5.2 0.9 2.2	
U== W== YZABBC ABBC	Fwd Power @ Input Power @ Load ( Power Reflected @ Pwr Return @ Input Net Power Out @ I Power Xfr to Load Transfer Ratio Improvement (wa Shack SWR ==>>	(FWD) ant) Load (REF) nput (ant) (ant) (%) tts) (:>)	120.6 60.4 41.1 20.6 100 19.3 19.3 3.3 <1:1>	253.8 239.6 163.0 153.8 100 76.7 76.7 46.5 <1:1>	Conj 111.2 55.7 22.3 11.2 100 33.4 33.4 33.4 3.4 4 .1:1>	ugate Mat 245.3 228.9 155.6 145.3 100 73.2 73.2 43.4 <1:1>	ch 113.5 56.9 27.0 13.5 100 29.9 29.9 3.6 <1:1>	
	NOTES ==>> maximum source ==>> INPUT paramet ==>> A is always n ==>> B is the char ==>> The load (ant and D = X, th ==>> ALL output ==>> E changes onl ==>> F changes onl i.e F changes onl or when eithe	e power ers are on-nega acteris ) imped e react values y when y when y when r load	is take A, B, C tive. It tic impe lance is ance. are dete the line either Z the char R (resis	n to be and D. is the dance Z Z = R + rmined loss/a o or Z acteris tance)	100 watt total fe o=Ro+j0 o jX. C by values ttenuatic (=R + jX) tic imped or X (rea	E and F. (= %pow () f the fee () f the fee	ver) ss in dB dline resistan <<<=== inges Ro) chan changes.	ce ges

#### nfarltop[1]

#### nfarlbot[1]

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EQUATIONS for Power Transfer Worksheet
E = 10pwr(-A/10) = 10^{(-A/10)}
F = SQRT[(B-C)^2 + D^2]/SQRT[(B+C)^2 + D^2]
G = (1+F)/(1-F)
H = E^*F
I = (1+H)/(1-H) = (1+(E*F))/(1-(E*F))
J = 100
K = F^{*}
L = K^{*}(F^{2}) = 100^{*}E^{*}(F^{2})
M = E^{*}L = 100^{*}(E^{*}F)^{2}
N = J-M = 100*(1-(E*F)^2)
P = K-L = 100 * E * (1 - (F^2))
Q = 100*(P/N) = 100*E*(1-F^2)/(1-(E*F)^2)
R = 10*LOG(N/P) = A + LOG[(1-F^2)/(1-(E*F)^2)]
S = R/6
T = R-A = LOG[(1-F^2)/(1-(E*F)^2)]
U = \frac{100}{(1 - (E^*F)^2)}
V = E^*U = 100^*E/(1-(E^*F)^2)
W = V * F^2 = 100 * E^{(F^2)/(1-(E*F)^2)}
X = E^*W = \frac{100^*((E^*F)^2)}{(1 - (E^*F)^2)}
Y = U - X = 100
Z = V^{*}(1-F^{2}) = 100^{*}E^{*}(1-F^{2})/(1-(E^{*}F)^{2}) = Q = AA
AA = 100 \times Z/Y = 100 \times E \times (1 - F^2) / (1 - (E \times F)^2) = Q = AA
BB = Z - P = \frac{100 (E^{3}) (F^{2}) (1 - F^{2})}{(1 - (E^{*}F)^{2})}
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#### nfarl1[1]

==>> note ==>>	==>> nfarl:	==>> 102'g	Power 5rv ape	xfr Wo x@50 e	rksheet nds@24.9	<<== angle	<<== 120deg	<<== gs
<pre>Freq (mhz) ==&gt;&gt;</pre>	28	24	21	18	14	10	7	3.5
Total Line Attn (dB) Line (Zo) ohms Load (R) ohms Load (X) ohms	0.58 300.0 3390.0 738.0	0.51 300.0 143.0 274.0	$0.44 \\ 300.0 \\ 365.0 \\ 1169.0$	0.45 300.0 1972.0 1918.0	0.39 300.0 114.0 -142.0	0.32 300.0 1898.0 2221.0	$0.26 \\ 300.0 \\ 508.0 \\ 1138.0$	0.17 300.0 2808.0 -249.0
Line Loss Factor Refl Coeff@Load(ant) Load SWR (@ant) Refl Coeff @ Input Input SWR (@shack)	0.875   0.844   11.84   0.739   6.65	0.889 0.606 4.08 0.539 3.34	0.904 0.871 14.45 0.787 8.38	0.902 0.856 12.87 0.772 7.75	$0.914 \\ 0.535 \\ 3.30 \\ 0.489 \\ 2.91$	0.929 0.876 15.08 0.813 9.72	0.942 0.829 10.69 0.781 8.12	0.962 0.808 9.43 0.777 7.98
Fwd Pwr@Input (FWD) Pwr@Load(ant) Pwr Refltd@Load Pwr Refltd@Load	100.0 87.5 62.4 54 6	100.0 88.9 32.7 29.1	NO 0 100.0 90.4 68.5	onjugat 100.0 90.2 66.0	te Match 100.0 91.4 26.1	100.0 92.9 71.2	100.0 94.2 64.7	100.0 96.2 62.8
Net Pwr Out@Input Pwr Xfr to Load(ant) Transfer Ratio (%) Pwr Loss (dB) Pwr Loss (S-unit)	45.4 25.1 55.3 2.6 0.4	70.9 56.2 79.3 1.0 0.2	38.1 21.9 57.4 2.4 0.4	40.5 24.1 59.6 2.2 0.4	76.1 65.3 85.8 0.7 0.1	33.8 21.7 64.0 1.9 0.3	39.0 29.5 75.5 1.2 0.2	39.6 33.3 84.2 0.7 0.1
Mismatch Loss(dB)	2.0	0.5	2.0	1.8	0.3	1.6	1.0	0.6
Fwd Pwr@Input(FWD) Pwr @ Load (ant) Pwr Refltd@Load Pwr Return@Input(REF) Net Pwr Out@Input Pwr Xfr to Load(ant) Transfer Ratio (%) Improvement (watts) Shack SWR ==>>(:>)	220.1 192.6 137.3 120.1 100 55.3 55.3 30.2 <1:1>	141.0 125.3 46.1 41.0 100 79.3 79.3 23.0 <1:1>	262.4 237.1 179.7 162.4 100 57.4 57.4 35.5 <1:1>	247.1 222.8 163.1 147.1 100 59.6 59.6 35.5 <1:1>	Match 131.4 120.1 34.3 31.4 100 85.8 85.8 20.5 <1:1>	295.6 274.6 210.5 195.6 100 64.0 64.0 42.4 <1:1>	256.1 241.2 165.7 156.1 100 75.5 75.5 46.0 <1:1>	252.6 242.9 158.7 152.6 100 84.2 84.2 84.2 50.9 <1:1>

0



**Loop SkyWire Showing Different Feed Points** 

EZNEC Pro/2

3.8 MHz

EZNEC Pro/2

3.8 MHz

92.0 deg.

6.73 dBi

0.0 dBmax

225.0 deg.

0.0 dBmax

3.52 dBi



Azimuth Plot

Outer Ring

Elevation Angle 16.0 deg.



14.2 MHz

40.0 deg.

8.69 dBi

0.0 dBmax

Cursor Az

Gain

45.0 deg.	Azimuth Plot
10.59 dBi	Elevation Angle
0.0 dBmax	Outer Ring

Slice Max Gain

Sidelobe Gain

Front/Sidelobe 0.0 dB

Front/Back

Beamwidth

16.0 deg.

8.69 dBi

1.7 dB

8.69 dBi @ Az Angle = 40.0 deg.

30.3 deg.; -3dB @ 24.5, 54.8 deg.

8.69 dBi @ Az Angle = 140.0 deg.

 Slice Max Gain
 10.59 dBi @ Az Angle = 45.0 deg.

 Front/Back
 2.65 dB

 Beamwidth
 33.6 deg.; -3dB @ 28.2, 61.8 deg.

 Sidelobe Gain
 9.95 dBi @ Az Angle = 135.0 deg.

 Front/Sidelobe
 0.64 dB

10.59 dBi

80-Meter Loop Corner Feed on 14.2 MHz 80-Meter Loop Center of Leg on 14.2 MHz

Cursor Az

Gain

#### Impedance = 513.1 - J 938.9 ohms



#### Impedance = 454.8 - J 994.8 ohms



EZNEC Pro/2



Azimuth Plot Azimuth Plot Cursor Az 58.0 deg. Elevation Angle 11.0 deg. Gain 10.63 dBi Elevation Angle 11.0 deg. 14.2 dBi Outer Ring Outer Ring 10.63 dBi 0.0 dBmax Slice Max Gain 14.2 dBi @ Az Angle = 45.0 deg. Slice Max Gain 10.63 dBi @ Az Angle = 58.0 deg. Front/Back 2.13 dB Front/Back 5.59 dB Beamwidth 22.8 deg.; -3dB @ 33.6, 56.4 deg. Beamwidth 19.9 deg.; -3dB @ 47.8, 67.7 deg. Sidelobe Gain 12.07 dBi @ Az Angle = 225.0 deg. Sidelobe Gain 10.63 dBi @ Az Angle = 122.0 deg

0.0 dB

Front/Sidelobe

21.3 MHz

45.0 deg. 14.2 dBi

0.0 dBmax

Cursor Az

Gain

Front/Sidelobe 2.13 dB Loop SkyWire Feed on 21.3 MHz